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Chip shape analysis during dry machining of nodular cast iron

Rüstem Binali^{*1}, Havva Demirpolat², Mustafa Kuntoğlu³

¹Department of Mechanical Engineering, Faculty of Technology, Selcuk University, Turkey ²Department of Mechanical Engineering, Faculty of Technology, Selcuk University, Turkey ³Department of Mechanical Engineering, Faculty of Technology, Selcuk University, Turkey <u>*rustem.binali@selcuk.edu.tr</u> Email of the corresponding author

Abstract – Chip shape in machining of metals not only reflects the quality and success of the operation but also carries the signs about the cutting mechanism. Most importantly, chips are responsible for the heat removal from the cutting zone which directly eliminates the thermal effects such as fatigue, shock, and early failure of edge due to excessive wear. Therefore, analysis of the chips is not only important in these aspects but also have significance in determination of the cutting parameters, lubricating and cooling conditions. This study addresses mentioned points by evaluating the milling parameters under dry cutting conditions to compare chip properties such as color, length, and helix etc. The evaluation was carried out by examining the microscopic images according to the experimentally obtained chips under two different levels of cutting speed, feed rate and depth of cut. The results of this experimental work are expected to be an idea for the future studies in the metal cutting sector.

Keywords - Chip Analysis, Cast Iron, Dry Cutting, Milling, Machinability

I. INTRODUCTION

Ductile (nodular) cast iron material is preferred in especially automotive industry due to their high strength and toughness and castability properties [1, 2]. Further, austempering process, which is consist of austenitizing, quenching, and transform of ferrite and austenite with different temperature and time conditions, enhance the mechanical properties of cast irons [3, 4]. In addition, it has low material cost, low production cost, low density and good machinability advantages [5]. But fast wear of cutting tools is a critical problem for machining of ductile cast iron [6]. Ghani et al. conducted an experimental study on nodular cast iron to explain the changing surface finish under the different cutting conditions. The results show that the ceramic tools are insufficient in terms of tool life [7]. Şeker and Hasırcı evaluated the surface finish and cutting force of ductile iron. It is revealed that the higher surface quality can be

obtained under the low cutting speed conditions [8]. Long analyzed the influence of cutting speed on tool life, surface roughness, and chip formation during turning with coated carbide tools. It was stated that the tool wear rate increases with increasing cutting speed and c-shaped the discontinuous chip formation was obtained for all grade of ductile iron [9]. Chip formations are classified as continuous, discontinuous and build up edge (BUE) [10]. Continuous chip formation can lead to deterioration of the surface quality and an increase in the temperature of the cutting tool when high-speed machining of ductile materials [11, 12]. The environmental machining is a critical aspect of manufacturing. It is ensured that the need for lubricant is reduced in dry or near-dry machining. Meena and Mansori conducted an experimental study on dry machining of ductile cast iron. The results of experiments showed that the low feed rate and higher cutting speed leads to

higher cutting force and higher mechanical and thermal loads on the cutting edge of tool. The segmented chip formation revealed with higher cutting speed. The failure of tools was obtained such as flank wear, crater wear, chipping, breakage and BUE. Chip morphology and tool wear were evaluated by surface roughness analysis [13]. The formation of chips and removing this material from the workpiece affect the surface finish quality [14]. The shape of chips are strictly related to microstructure and mechanical properties of workpiece material and cutting conditions [15]. Yazman et al. evaluated the chip morphology based on cutting speed. It was reported that the highest BUE was observed under the low cutting speed condition and unstable BUE was observed with increasing cutting speed. Long and helical chip patterns was specified in high cutting speed conditions [16].

Chip formation has an impact on the surface finish quality and tool wear.

As seen, chip analysis was done before from the researchers in the field for different types of materials. The main objective of this study is to investigate the chip shape of nodular cast iron during dry machining. In this direction,

II. MATERIALS AND METHOD

GGG50 nodular cast iron specimens were used in tests that chemical composition is seen in Table 1. The dimensions of the workpiece billets were 30 mm width and 100 mm in length. TiC coated CCMT 09T308-304 series cutting tool was used. Cutting tools were renewed after every try. Tests were conducted with a three axis CNC milling (SUNMILL) machine with different cutting parameters as specified in Table 2. The full factorial method was used in designing the tests. Chips were evaluated based on different cutting conditions.

Table 1 Chemical composition of GGG 50 specimen	s.
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Table 1 Chemical composition of GGG 50 specimens.								
Element	С	Si	Mn	Mg	Р	S		
	wt%	wt%	wt%	wt%	wt%	wt%		
GGG50	3.5-	2-3	0.4	0.06-	0.1	0.01		
	3.8			0.12				
Table 2. The parameters of milling								
	Table	e 2. The p	parameter	rs of mill	ing			
Cutting	Table Speed	e 2. The p Feed S	oarameter Speed	rs of mill Cutt	ing ing Dep	oth		
Cutting (m/m	Table Speed in)	e 2. The p Feed S (mm/	oarameter Speed (rev)	rs of mill Cutt	ing ing Der (mm)	oth		
Cutting (m/m 150-2	Table Speed in) 200	e 2. The p Feed S (mm/ 0.15	barameter Speed (rev) -0.3	rs of mill Cutt	ing ing Dep (mm) 0.2-0.4	oth		

III. RESULTS

Chip analysis is highly important in machining due to the listed reasons:

i) Chips can remove the excessive heat from the cutting zone which makes it critical to elongate the cutting tool life by eliminating accelerated tool wear and reduced mechanical properties of the work material.

ii) Ideally, chips are expected to break by the natural flow of the machining process. There are two undesired ways for breakage of the chips such as breaking by crashing to cutting tool or workpiece. In these scenarios, there is possibility to make damage on cutting tool edge or workpiece surface. Therefore, breakage of chips by itself not guarantees the desired chip shape but increases the possibility in obtaining the desired form.

iii) When stable chip breakage can be carried out during machining, same quality indicators of the workpiece through all faces such as surface roughness, dimensional accuracy and surface topography can be obtained. This is highly criticial to reach sustainable and reliable manufacturing.

iv) Since the metal cutting is an art of the chip formation, all basic mechanisms around the cutting zone is related with the chip shape. Therefore, understanding of the chip shape opens new doors in the way of improved machinability.

Figure 1 represents the chips obtained from the experiments. Some examples taken from the group of chips are demonstrated in here. Also, cutting parameters are given at the top of the figures. Milling experiments can generate short chips as per the cutting mechanism. Especially, in the perspective of this study, a brittle material was used. Brittle materials are expected to produce serrated and short chips. From this point of view, it can be clearly seen that 8 chips in the figures have serrations. Some serrations look much more deeper which are generally at lower cutting speeds namely 150 m/min. On the other hand, chips may have different shapes such as c, comma, curled. Especially in the curved type, helix number may be higher which is an undesired situation due to the reason of heat accumulation at the contact surfaces between chip and tool or chip and workpiece. When looking at the chips morphology, higher feed rate namely 0.3 mm/tooth is much better than the lower value in this perspective. Seemingly, depth of cut has no important effect on the chip shape. When looking at the colors of the chips, no big difference was seen. It should be noted that chip shapes may show differences from starting point to the finish of the machining.



Figure 1. Chips obtained from the experiments.

IV. CONCLUSION

The observations of this study can be listed in the following:

- Seemingly, depth of cut has no important effect on the chip shape.
- 8 chips obtained from milling of the cast iron in the figures have serrations.
- Higher feed rate namely 0.3 mm/tooth is much better than the lower value.
- Some serrations look much deeper which are generally at lower cutting speeds namely 150 m/min.
- When looking at the colours of the chips, no big difference was seen.

References

1. Guzel, E.; Yuksel, C.; Bayrak, Y.; Sen, O.; Ekerim, A., Effect of section thickness on the microstructure and hardness of ductile cast iron. *Materials Testing* **2014**, 56, (4), 285-288.

Bosnjak, B.; Asanovic, V.; Radulovic, B.; Pop-Tonev, K., Influence of microalloying and heat treatment on the kinetics of bainitic reaction in austempered ductile iron. *Journal of Materials Engineering and Performance* **2001**, 10, (2), 203-211.

2.

- Keough, J. R.; Hayrynen, K. L., Automotive applications of austempered ductile iron (ADI): a critical review. *SAE transactions* **2000**, 344-354.
- Kilinc, B.; Kirtay, S., Influence of Cu addition and austempering treatment on mechanical properties and microstructure of GGG 50. *Acta Physica Polonica A* **2017**, 132, (3), 461-465.
- Rao, P. P.; Putatunda, S. K., Investigations on the fracture toughness of austempered ductile irons austenitized at different temperatures. *Materials Science and Engineering: A* **2003**, 349, (1-2), 136-149.
- Del Val, A. G.; Alonso, U.; Veiga, F.; Arizmendi, M., Wear mechanisms of TiN coated tools during high-speed tapping of GGG50 nodular cast iron. *Wear* **2023**, 514, 204558.
- Ghani, A.; Choudhury, I., Study of tool life, surface roughness and vibration in machining nodular cast iron with ceramic tool. *Journal of Materials Processing Technology* **2002**, 127, (1), 17-22.
- Şeker, U.; Hasirci, H., Evaluation of machinability of austempered ductile irons in terms of cutting forces and surface quality. *Journal of Materials Processing Technology* **2006**, 173, (3), 260-268.
- Ting, P. L., A Study of the Turning of Austempered Ductile Iron (ADI) Grades with Coated Carbide Tools. **2016**.
- Yılmaz, B.; Karabulut, Ş.; Güllü, A., A review of the chip breaking methods for continuous chips in turning. *Journal of Manufacturing Processes* 2020, 49, 50-69.
- 11. Rahman, M.; Seah, K.; Li, X.; Zhang, X., A threedimensional model of chip flow, chip curl and chip breaking under the concept of equivalent parameters. *International Journal of Machine Tools and Manufacture* **1995**, 35, (7), 1015-1031.
- Yazman, Ş.; Akdemir, A.; Uyaner, M.; Bakırcıoğlu, B. In *The Effect of Build Up Edge Formation on the Machining Characteristics in Austempered Ferritic Ductile Iron*, ASME International Mechanical Engineering Congress and Exposition, 2013; American Society of Mechanical Engineers: 2013; p V02BT02A052.
- 13. Meena, A.; El Mansori, M., Specific cutting force, tool wear and chip morphology characteristics during dry drilling of austempered ductile iron (ADI). *The International Journal of Advanced Manufacturing Technology* **2013**, 69, (9-12), 2833-2841.
- Su, G.; Liu, Z.; Li, L.; Wang, B., Influences of chip serration on micro-topography of machined surface in high-speed cutting. *International Journal of Machine Tools and Manufacture* 2015, 89, 202-207.

- Salem, S. B.; Bayraktar, E.; Boujelbene, M.; Katundi, D., Effect of cutting parameters on chip formation in orthogonal cutting. *Journal of Achievements in Materials and manufacturing Engineering* 2012, 50, (1), 7-17.
- Yazman, Ş.; Gemi, L.; Uludağ, M.; Akdemir, A.; Uyaner, M.; Dişpinar, D., Correlation between machinability and chip morphology of Austempered ductile iron. J. Test. Eval 2017, 46, (3), 1012-1021.